MSK

H-BRIDGE **3014** MOSFET POWER MODULE

M.S.KENNEDY CORP.

4707 Dey Road Liverpool, N.Y. 13088

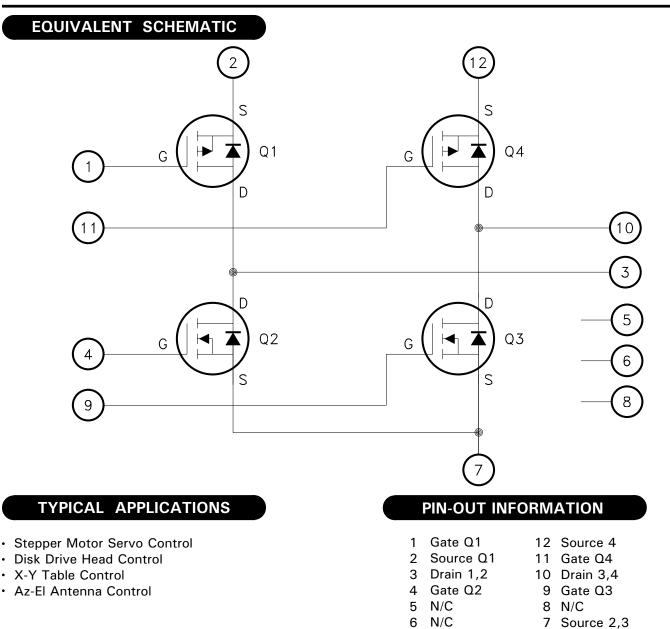
FEATURES:

- P and N Channel MOSFETs for Ease of Drive
- 100 Volt, 10 Amp Full H-Bridge
- · Isolated Package for Direct Heat Sinking, Excellent Thermal Conductivity
- Avalanche Rated Devices

(315) 701-6751

DESCRIPTION:

The MSK 3014 is an H-bridge power circuit packaged in a space efficient isolated ceramic tab power SIP package. The MSK 3014 consists of P-Channel MOSFETs for the top transistors and N-Channel MOSFETs for the bottom transistors. The MSK 3014 uses M.S. Kennedy's proven power hybrid technology to bring a cost effective high perfomance circuit for use in today's sophisticated servo motor and disk drive systems.



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ABSOLUTE MAXIMUM RATINGS

VDSS	Drain to Source Voltage100V MAX			
Vdgdr	Drain to Gate Voltage			
	$(RGS = 1M\Omega)$			
Vgs	Gate to Source Voltage			
	(Continuous) ± 20V MAX			
ID	Continuous Current			
IDM	Pulsed Current			
Rth-JC	Thermal Resistance			
	(Junction to Case)			

ELECTRICAL SPECIFICATIONS

	Single Pulse Avalanche Energy		
	(Q2,Q4,Q6)		
	(Q1,Q3,Q5)		
Тı	Junction Temperature + 175°C MAX		
Тsт	Storage Temperature		
Tc	Case Operating Temperature Range -55°C to +125°C		
Tld	Lead Temperature Range		
	(10 Seconds)		

Parameter	Test Conditions ④	MSK3014			
raiametei	Test Conditions (4)	Min.	Тур.	Max.	Units
Drain-Source Breakdown Voltage	$V_{GS} = 0$ ID = 0.25mA (All Transistors)	100	-	-	V
Durin Course Lookana Current	$V_{DS} = 100V V_{GS} = 0V (Q2,Q3)$	-	-	25	μA
Drain-Source Leakage Current	$V_{DS} = -100V V_{GS} = 0V (Q1,Q4)$	-	-	-25	μA
Gate-Source Leakage Current	$V_{GS} = \pm 20V V_{DS} = 0$ (All Transistors)	-	-	±100	nA
Gate-Source Threshold Voltage	$V_{DS} = V_{GS}$ ID = 250 μ A (Q2,Q3)	2.0	-	4.0	V
Gate-Source Threshold Voltage	$V_{DS} = V_{GS}$ ID = 250 μ A (Q1,Q4)	2.0	-	4.0	V
Droin Source On Registeres	$V_{GS} = 10V I_D = 9.0A (Q2,Q3)$	-	-	0.20	Ω
Drain-Source On Resistance (2)	$V_{GS} = -10V \ I_D = -8.4A \ (Q1,Q4)$	-	-	0.28	Ω
Drein Source On Projetance	$V_{GS} = 10V I_D = 9.0A (Q2,Q3)$	-	-	0.11	Ω
Drain-Source On Resistance ③	$V_{GS} = 10V I_D = -8.4A (Q1,Q4)$	-	-	0.20	Ω
Forward Transmission (1)	$V_{DS} = 50V I_{D} = 9.0A (Q2,Q3)$	6.4	-	-	S
Forward Transconductance (1)	VDS = -50V ID = -8.4A (Q1,Q4)	3.2	-	-	S
N-Channel (Q2,Q3)					
Total Gate Charge ①	ID = 9.0A	-	-	44	nC
Gate-Source Charge ①	Vds = 80V	-	-	6.2	nC
Gate-Drain Charge ①	$V_{GS} = 10V$	-	-	21	nC
Turn-On Delay Time ①	$V_{DD} = 50V$	-	6.4	-	nS
Rise Time ①	ID = 9.0A	-	27	-	nS
Turn-Off Delay Time (1)	$R_G = 12\Omega$	-	37	-	nS
Fall Time (1)	$R_D = 5.5\Omega$	-	25	-	nS
Input Capacitance ①	V _{GS} = 0V	-	640	-	pF
Output Capacitance ①	Vds = 25V	-	160	-	pF
Reverse Transfer Capacitance (1)	f = 1.0MHz	-	88	-	pF
P-CHANNEL (Q1,Q3,Q5)					
Total Gate Charge ①	ID = -8.4A	-	-	58	nC
Gate-Source Charge ①	Vds = -80V	-	-	8.3	nC
Gate-Drain Charge ①	Vgs=-10V	-	-	32	nC
Turn-On Delay Time ①	Vdd = -50V	-	15	-	nS
Rise Time ①	$I_{D} = -8.4A$	-	58	-	nS
Turn-Off Delay Time ①	$R_G = 9.1\Omega$	-	45	-	nS
Fall Time ①	$R_D = 6.2\Omega$	-	46	-	nS
Input Capacitance ①	Vgs=0V	-	760	-	pF
Output Capacitance ①	VDS = -25V	-	260	-	pF
Reverse Transfer Capacitance ①	f = 1.0MHz	-	170	-	pF
BODY DIODE					
Forward On Voltage ①	Is=9.0A VGs=0V (Q2,Q3)	-	1.3	-	V
	Is=-8.4A VGs=0V (Q1,Q4)	-	-1.6	-	V
Reverse Recovery Time (1)	$Is = 9.0A \ di/dt = 100A/\mu S \ (Q2,Q3)$	-	130	190	nS
	$Is = -8.4A \ di/dt = 100A/\mu S \ (Q1,Q4)$	-	130	190	nS
Reverse Recovery Charge (1)	$Is = 9.0A \ di/dt = 100A/\mu S \ (Q2,Q3)$	-	650	970	μC
neverse necovery charge ()	$Is = -8.4A \text{ di/dt} = 100A/\mu S (Q1,Q4)$	-	650	970	μC

NOTES:

 1 This parameter is guaranteed by design but need not be tested. Typical parameters are representative of actual device performance but are for reference only.

 (2) Resistance as seen at package pins.

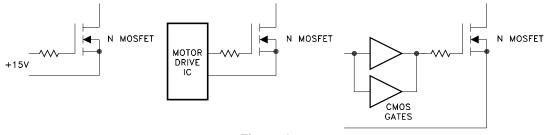
 (3) Resistance for die only; use for thermal calculations.

 (4) TA = 25 °C unless otherwise specified.

APPLICATION NOTES

N-CHANNEL GATES (02,03)

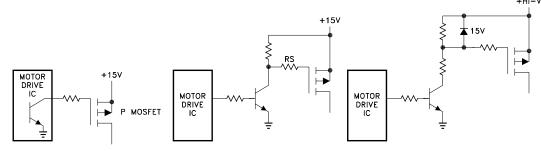
For driving the N-Channel gates, it is important to keep in mind that it is essentially like driving a capacitance to a sufficient voltage to get the channel fully on. Driving the gates to +15 volts with respect to their sources assures that the transistors are on. This will keep the dissipation down to a minimum level [RDs(ON) specified in the data sheet]. How quickly the gate gets turned ON and OFF will determine the dissipation of the transistor while it is transitioning from OFF to ON, and vice-versa. Turning the gate ON and OFF too slow will cause excessive dissipation, while turning it ON and OFF too fast will cause excessive switching noise in the system. It is important to have as low a driving impedance as practical for the size of the transistor. Many motor drive IC's have sufficient gate drive capability for the MSK 3014. If not, paralleled CMOS standard gates will usually be sufficient. A series resistor in the gate circuit slows it down, but also suppresses any ringing caused by stray inductances in the MOSFET circuit. The selection of the resistor is determined by how fast the MOSFET wants to be switched. See Figure 1 for circuit details.





P-CHANNEL GATES (Q1,Q4)

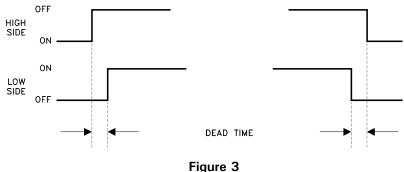
Most everything applies to driving the P-Channel gates as the N-Channel gates. The only difference is that the P-Channel gate to source voltage needs to be negative. Most motor drive IC's are set up with an open collector or drain output for directly interfacing with the P-channel gates. If not, an external common emitter switching transistor configuration (see Figure 2) will turn the P-Channel MOSFET on. All the other rules of MOSFET gate drive apply here. For high supply voltages, additional circuitry must be used to protect the P-Channel gate from excessive voltages.





BRIDGE DRIVE CONSIDERATIONS

It is important that the logic used to turn ON and OFF the various transistors allow sufficient "dead time" between a high side transistor and its low side transistor to make sure that at no time are they both ON. When they are, this is called "shoot-through", and it places a momentary short across the power supply. This overly stresses the transistors and causes excessive noise as well. See Figure 3.

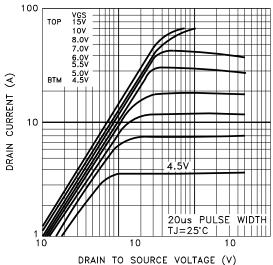


This deadtime should allow for the turn on and turn off time of the transistors, especially when slowing them down with gate resistors. This situation will be present when switching motor direction, or when sophisticated timing schemes are used for servo systems such as locked antiphase PWM'ing for high bandwidth operation.

TYPICAL PERFORMANCE CURVES

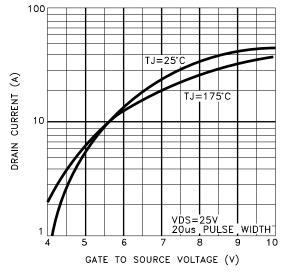
N-CHANNEL DEVICES (Q2,Q3)

DRAIN CURRENT vs DRAIN TO SOURCE VOLTAGE

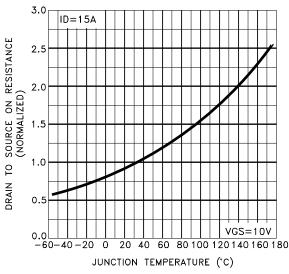


DIVAIN TO SOURCE VULLAGE (V)



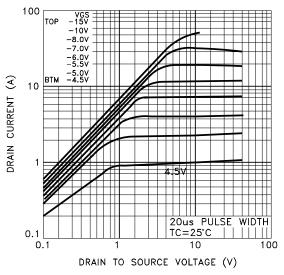


DRAIN TO SOURCE ON RESISTANCE vs JUNCTION TEMP.

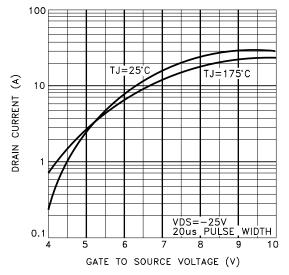


P-CHANNEL DEVICES (Q1,Q4)

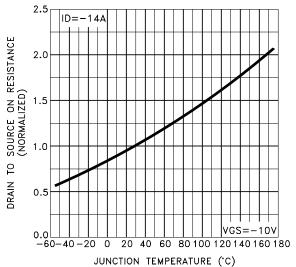
DRAIN CURRENT VS DRAIN TO SOURCE VOLTAGE



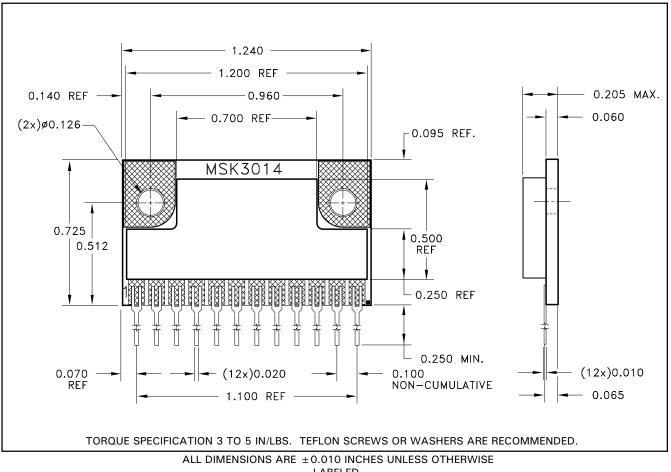
DRAIN CURRENT vs GATE TO SOURCE VOLTAGE



DRAIN TO SOURCE ON RESISTANCE vs JUNCTION TEMP.



MECHANICAL SPECIFICATIONS



LABELED.

ORDERING INFORMATION

PART NUMBER	SCREENING LEVEL	
MSK 3014	Industrial	

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